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## Original Article

Tailoring optical and resistance properties of the functional  $\text{CuAl}_x\text{O}_y$  semiconductor for applications as thermal infrared imagers

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## ABSTRACT

This is the first report on the optical and resistance properties of copper aluminum oxide thin films for applications as thermal infrared imagers. The deposition of these films was investigated under three series of reactive magnetron sputtering conditions. Structural characterization identified the P63mm hexagonal crystalline structure of  $\text{CuAlO}_2$  although the 150- to 350-nm thick films were in a non-stoichiometric  $\text{CuAl}_x\text{O}_y$  ratio. The thermal coefficient of resistance of the  $\text{CuAl}_x\text{O}_y$  films was measured to be in the range 1.7–2.2%/K and the resistivity ranged from 0.3 to 1.0  $\Omega$  cm with n-type nature. To explain the low indirect bandgap value of the  $\text{CuAl}_x\text{O}_y$  films, a type-I band alignment bulk heterojunction between  $\text{CuAlO}_2$  and  $\text{Cu}_2\text{O}$  is proposed. This provides an effective method to decrease the resistivity and increase the thermal coefficient of resistance. From their optical characterization, a refractive index of  $2.27 \pm 0.07$  was deduced, thus favoring the  $\text{CuAl}_x\text{O}_y$  films for antireflection coating in the long infrared wavelength region. A micromachining process of  $\text{CuAl}_x\text{O}_y$  micro-bridges was demonstrated with well-defined shapes at a pixel pitch of 25  $\mu\text{m}$ . These findings pave the way for the future development of high-performance thermal infrared imagers.

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## 1. Introduction

Uncooled thermal infrared imagers, or uncooled focal plane arrays (UFPAs), are devices allowing us to capture the temperature distribution of a scene without cooling. Since their inception, UFPAs were not believed to be competitive against cooled thermal

infrared imagers because of their limited ability to simultaneously improve spatial resolution and temperature resolution [1]. Nevertheless, thanks to their room temperature operation, UFPAs have gained tremendous attention as well as a very large spectrum of applications [2]. The fabrication of UFPAs relies heavily on surface micromachining technology, which in turn has been leveraged by the development of the complementary metal oxide semiconductor (CMOS) industry [3–5]. The technological readiness of UFPAs is at a very high level [6] with the participation of very active main players in the market [7–12]. However, newcomers are willing to enter the market since the needs of UFPAs are quite specific regionally and nationally [13,14].

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The room temperature operation condition and the working mechanism of UFPAs require that they possess the following criteria: (i) high absorption of radiation in the long wavelength infrared region (LWIR), (ii) high thermal isolation of the sensing element, and (iii) high thermal coefficient of resistance (TCR) of the sensing element. Micro-devices composed of an UFPA, which have all of these three important criteria, are called micro-bolometers [6]. To attain high radiation absorption in the LWIR, micro-bolometers are often multilayered structures that act simultaneously in antireflection and absorption roles [15]. For high thermal isolation, micro-bolometers need to be suspended from the substrate carrying them [16]. A combination of absorption and suspension thus presents the idea of forming a quarter wavelength Fabry-Perot micro cavity in the thermal infrared region, whose central wavelength is around 10  $\mu\text{m}$  [17]. Lastly, the resistive sensing mechanism of a micro-bolometer requires a thin film material with a high TCR value. Candidates responding to this criterion are semiconductor materials having high activation energies [18].

For micro-bolometers, amorphous silicon is the conventional choice since it is compatible with CMOS technology and its resistivity can be tuned by doping, thus allowing a wide range of selection for fabrication process. Amorphous silicon is often deposited in thin film form [9]. Another famous candidate for the sensing layer of a micro-bolometer is vanadium oxide ( $\text{VO}_x$ ). The special property of  $\text{VO}_x$  is that vanadium possesses multiple oxidation states that inherently allow  $\text{VO}_x$  to shift its crystalline phase with changing temperature. As a result, the resistivity of  $\text{VO}_x$  changes accordingly with temperature, which leads to its high TCR value [19]. Together, amorphous silicon and  $\text{VO}_x$  are the main players in UFPA applications nowadays, however, there are still many choices for materials for the active layer of a micro-bolometer. For example, some choices are (i) ternary oxide semiconductor compounds like perovskites with a formula of  $\text{ABO}_3$  [20] or spinels with a formula of  $\text{AB}_2\text{O}_4$  [21], (ii) quaternary oxide compounds such as  $\text{YBaCuO}$  [22], (iii) composite graphene and carbon nanotubes based materials [23,24], and (iv) germanium-based materials [25].

There is another type of ternary compound semiconductor with a delafossite crystalline structure and formula of  $\text{ABO}_2$  where A is a monovalent and B is a trivalent metal cation that has been well known in the literature for being a wide band gap p-type semiconductor compound for applications in transparent conductive oxides [26–30]. There have been many reports on the electrical properties of  $\text{ABO}_2$  but a few of those have focused on its applications in micro-bolometers even though its temperature behavior of resistance was very interesting [31–34]. In this paper, we focus our efforts on a special type of a delafossite oxide semiconductor with a formula  $\text{CuAlO}_2$  for the development of thermal infrared imagers. In comparison to our previous study [35] reporting on  $\text{CuFeO}_2$ , we have replaced the trivalent metal cation  $\text{Fe}^{3+}$  with  $\text{Al}^{3+}$ . The reason behind this replacement is the behaviour of ferromagnetic Fe, which can cause unwanted effects when applying these films in optoelectronic applications. In addition, there is a special property of  $\text{CuAlO}_2$  in that the multi oxidation state of copper may allow  $\text{CuAlO}_2$  to tune its resistivity with temperature, thus promising a high TCR value. Herein, we present the first thorough investigation of the optical and resistance properties of  $\text{CuAlO}_2$  for applications as UFPAs. We demonstrate that the temperature behavior and refractive index at the LWIR of  $\text{CuAlO}_2$ , in combination with its capacity for surface micromachining fabrication, make it an excellent candidate as the active layer of a micro-bolometer.

## 2. Experimental

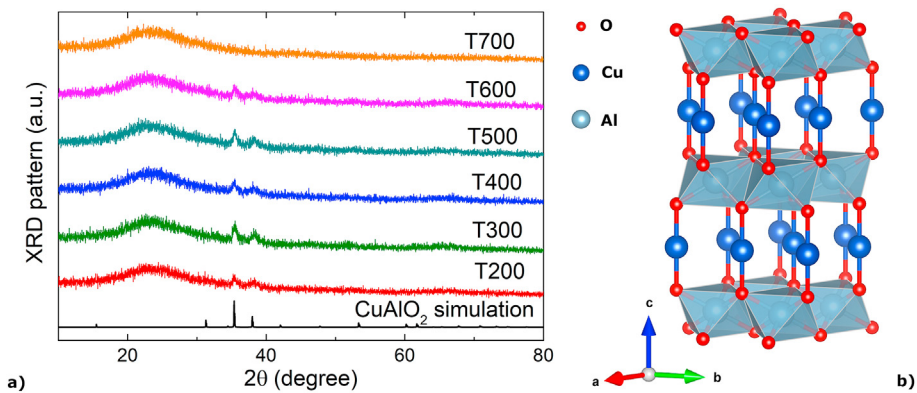
All  $\text{CuAl}_x\text{O}_y$  thin film samples were deposited by reactive magnetron sputtering. The sputtering system, from Syskey, has four

2-in magnetron guns with two direct current (DC) sources for metal deposition and two radio frequency (RF) sources for oxide target deposition. The detailed sputtering conditions are presented in Table S1. Three series of samples were investigated, including one with varying sputtering power of the  $\text{Cu}_2\text{O}$  target (denoted as  $\text{CuO-X}$ ), one with varying substrate temperature (denoted as TX00), and one with varying the sputtering power of both the  $\text{Cu}_2\text{O}$  and  $\text{Al}_2\text{O}_3$  targets (denoted as  $\text{AlCu-X}$ ).

The structural characterization of the thin film samples was carried out on an X-ray diffractometer (EQUINOX 5000, Thermo Scientific) with  $\text{Cu-K}_\alpha$  X-ray radiation at 1.54056 Å of wavelength. The surface quality was investigated on a scanning electron microscopy system (SEM) (S4800, Hitachi) with elemental analysis by energy-dispersive X-ray spectroscopy (EDX). The temperature-dependent electrical measurements were performed on a four-point probe system (RM300, Jandel) with additional characterization by a Keithley 2400 source measurement unit and a customized temperature controller from 10 °C to 50 °C. The Hall measurement was carried out on a Hall system with Van der Pauw configuration (7700 series, Lakeshore). The thicknesses of all samples were characterized on a stylus surface profilometer (NanoMap 500LS, AEP Technology). Optical characterization was carried out on an ultraviolet-visible (UV-VIS) spectrometer (UV-26000, Shimadzu) and spectroscopic ellipsometer (SE) (SmartSE, Horiba Jobin Yvon). The SE adjustment was performed with DeltaPsi software (Horiba Jobin Yvon) using a conventional model composed by a substrate, a bulk layer containing all information about the thin film, and a roughness layer (50% of the bulk material and 50% of void). The demonstration of surface micromachining was performed with a process flow consisting of eight optical lithography and etching steps prior to the final release of micro-bridges for forming the desired micro-bolometers.

## 3. Results and discussion

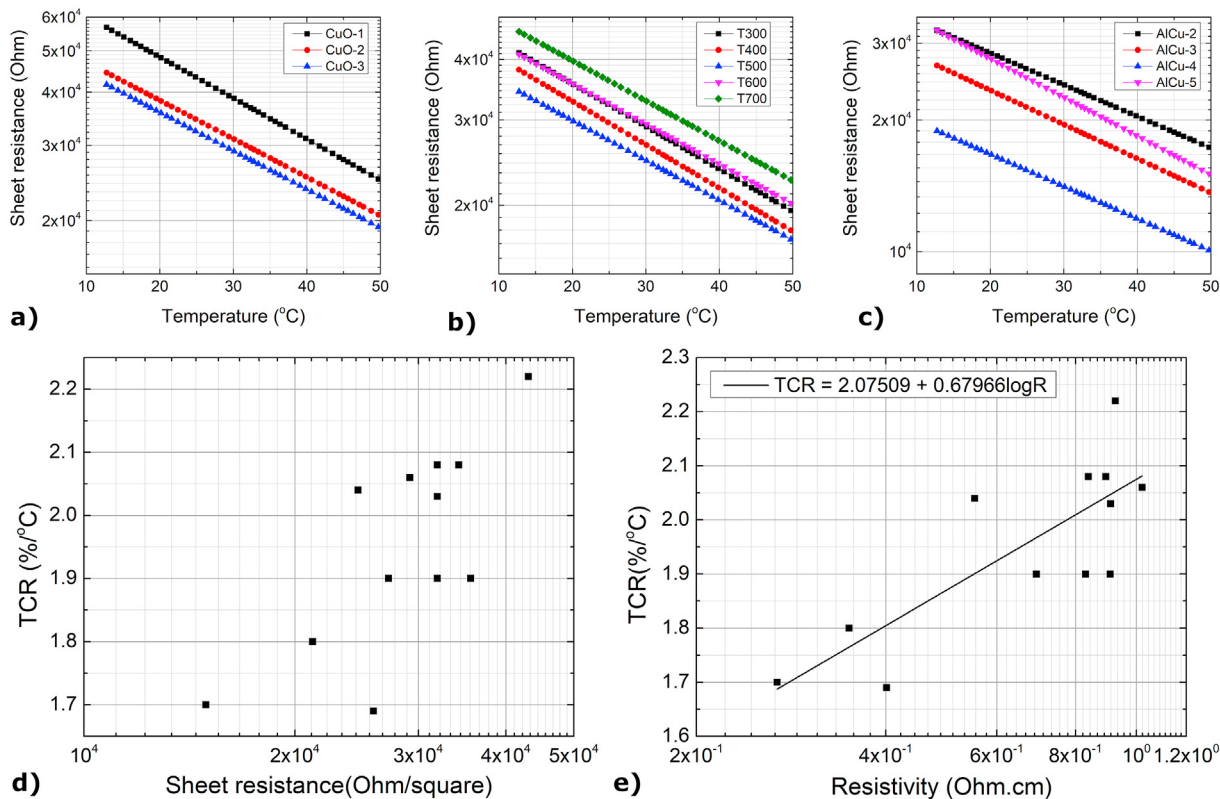
Fig. 1a shows X-ray diffraction (XRD) patterns of the samples in the temperature series (XRD patterns of the other two series are illustrated in Fig. S1). There are no significant XRD peaks observed on the patterns except for one at about 35.5° and 38°. Nevertheless, a Rietveld analysis was performed (the details are shown in Fig. S2) for sample T200 (the same as the sample  $\text{CuO-3}$ ) and allowed a decent structural extraction from the experimental XRD pattern. By using  $\text{CuAlO}_2$  with a hexagonal crystalline structure with the space group  $\text{P63mmc}$ , known as the delafossite structure, the Rietveld refinement gave the lattice parameters of  $a = b = 3.0029$  Å and  $c = 11.4212$  Å (angles  $\alpha = \beta = 90^\circ$  and  $\gamma = 120^\circ$  are fixed by the space group  $\text{P63mmc}$ ). As a result, we identified that the XRD peak at 35.5° corresponded to (101) reflection plane and the one at 38° corresponded to the (102) reflection plane of hexagonal  $\text{P63mmc}$ , which is quite similar to that reported in the literature [36]. The XRD patterns of other samples (except sample T700) of this temperature series exhibit the same feature, indicating that they share the same delafossite  $\text{CuAlO}_2$  crystalline structure. The unit cell of this structure is presented in Fig. 1b (the detailed positions of each atom are provided in Table S2). We can easily recognize the usual layered structure of the delafossite  $\text{ABO}_2$  (A is a monovalent and B is a trivalent metal cation) structure illustrated by the sandwiching of edge sharing  $\text{Al}_2\text{O}_3$  octahedral layers and  $\text{Cu}_2\text{O}$  layers. In order to check if another crystalline phase of a copper aluminum oxide, copper oxide, or aluminum oxide compound individually exists in the thin films, a comparison with XRD powder patterns of those oxides is presented in Fig. S3. The result shows that the two intense peaks, 35.5° for (101) and 38° for (102), are by far best described by the delafossite  $\text{CuAlO}_2$  hexagonal structure.



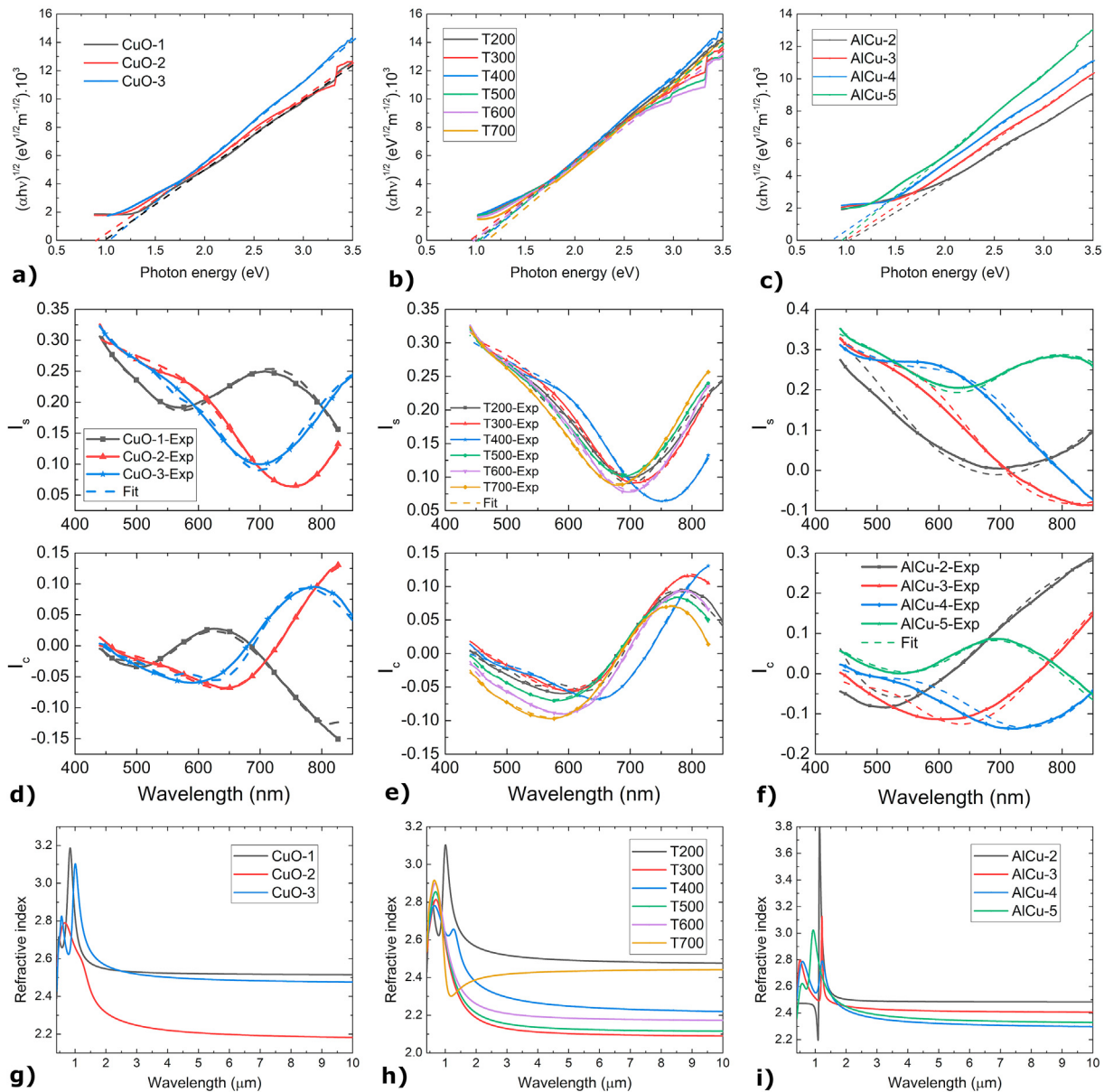
**Fig. 1.** (a) XRD patterns of the temperature series in comparison with the powder XRD simulation of CuAlO<sub>2</sub> based on the lattice parameters obtained from the Rietveld XRD refinement of sample T200 (details shown in Fig. S2). (b) The unit cell of the CuAlO<sub>2</sub> P63mmc hexagonal structure (details shown in Table S2) where the red atoms are oxygen, blue atoms are copper, and brown atoms are aluminum. Edge-sharing Al<sub>2</sub>O<sub>3</sub> octahedral layers are sandwiched by Cu<sub>2</sub>O layers.

Fig. 2 shows the temperature behavior of the resistance of all thin films in this study. For the temperature dependence from about 10 °C–50 °C, which is enough for uncooled infrared sensing applications, we observe a good linearity of the logarithm of the sheet resistance of the films as a function of temperature. This linearity is the basis for deducing the TCR values of the films, which are in the range from 1.7%/°C to 2.2%/°C (for simplicity here we refer to the absolute values of TCR instead of its real negative value). The semiconductor nature of the CuAl<sub>x</sub>O<sub>y</sub> films is confirmed by the fact that the sheet resistance decreases when increasing the temperature. We can see that for the series changing the sputtering power of the Cu<sub>2</sub>O target, when combined with the elemental

characterization by EDX shown in Table S3, the highest TCR value corresponds to the lowest concentration of copper. It is normal that this concentration increases when increasing the Cu<sub>2</sub>O target power but it is accompanied by a decrease of TCR value. For the substrate temperature series, the TCR value does decrease with increasing temperature. And for the third series, when the sputtering power of both oxide targets increases, the copper concentration increases and the TCR value becomes more important. Fig. 2d and e, respectively, show the dependency of TCR values with the sheet resistance and the resistivity of the CuAl<sub>x</sub>O<sub>y</sub> films. The sheet resistance is important when practically optimizing these CuAl<sub>x</sub>O<sub>y</sub> films for micro-bolometer applications, whereas the



**Fig. 2.** Temperature dependence of the sheet resistance of thin films from three series: (a) sputtering power of the Cu<sub>2</sub>O target, (b) sputtering temperature, (c) sputtering power of the Al<sub>2</sub>O<sub>3</sub> and Cu<sub>2</sub>O targets. Perfect linearity between the logarithm of the sheet resistance of the CuAl<sub>x</sub>O<sub>y</sub> thin films and the temperature is observed thus showing its advantage for micro-bolometer applications. (d) TCR values versus the sheet resistance at 30 °C and (e) TCR versus the resistivity at 30 °C for all samples in three series.

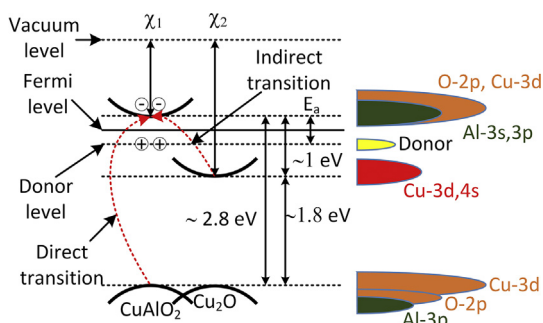


**Fig. 3.** (a)–(c) are the indirect band gap extrapolations of the  $\text{CuAl}_x\text{O}_y$  thin films of the three series. (d)–(f) are the comparison of  $I_s$  and  $I_c$  normalized experimental intensities (solid lines) and the corresponding SE adjustment intensities based on a double amorphous dispersion function (dashed lines) of the three series, and (g)–(i) are the extrapolation of the refractive indices to the long infrared wavelength region by using the extracted parameters of the double amorphous dispersion function for the three series.

resistivity is better for fundamental studies on the nature of the resistance property. Depending on the circuitry of the uncooled thermal infrared sensors, the resistance of a microbolometer is generally in the range of 25 k $\Omega$ –95 k $\Omega$ , thus giving a range of sheet resistance from 12.5 k $\Omega$ /square to 47.5 k $\Omega$ /square (suppose that the micro-bolometer is composed mainly of a rectangular  $\text{CuAl}_x\text{O}_y$  thin film with the width being half of the length). Fig. 2d shows that all  $\text{CuAl}_x\text{O}_y$  films of the three series well satisfy this resistance condition. On the other hand, we can observe that the  $\text{CuAl}_x\text{O}_y$  films deposited by sputtering in this study follow a general dependency between TCR values and resistivity, with higher resistivity producing higher TCR. In comparison to the resistivity of  $\text{VO}_x$ , which is in the range from 0.01 to 1  $\Omega\text{cm}$  [37], and to the resistivity of amorphous silicon, which is in the range from 100 to 10 k  $\Omega\text{cm}$  [9], the  $\text{CuAl}_x\text{O}_y$  films in this study lie in between 0.3 and 1.0  $\Omega\text{cm}$ . Furthermore, the Hall measurement with Van der Pauw pad

configuration for one selected sample per experimental series revealed a *n-type* semiconductor nature of  $\text{CuAl}_x\text{O}_y$ . A carrier concentration value of  $2.42 \times 10^{18} \text{ cm}^{-3}$  and a Hall mobility of  $6.48 \text{ cm}^2\text{V}^{-1}\text{s}^{-1}$  were found for CuO-3/T200 (TCR = 2.08%/°C) and a carrier concentration of  $8.58 \times 10^{18} \text{ cm}^{-3}$  and Hall mobility of  $4.08 \text{ cm}^2\text{V}^{-1}\text{s}^{-1}$  for AlCu-4 (TCR = 1.70%/°C). By fitting the temperature dependence of sheet resistance for all samples, the activation energy  $E_a$  was deduced, which ranged from 132 meV to 175 meV (a typical fit is shown in Fig. S5).

Based on the thickness measurements performed on the profilometer (shown in Table S3) there is another correlation that we can deduce from the XRD patterns: the thinner the sample, the more difficult to obtain the pronounced XRD peaks. As a matter of fact, no XRD peak is found (Fig. S1) for the samples from the series with varying sputtering power of both oxide targets because they are quite thin. Another question that can be raised is a correlation



**Fig. 4.** A proposed schematic of electronic levels and PDOS of  $\text{CuAl}_x\text{O}_y$  by considering phases of  $\text{CuAlO}_2$  and  $\text{Cu}_2\text{O}$  in an amorphous matrix. In the intrinsic p-type nature, the electronic affinity of  $\text{CuAlO}_2$   $\chi_1$  is 2.5 eV and that of  $\text{Cu}_2\text{O}$   $\chi_2$  is 3.2 [39,40]. When doped with donors, these affinities would increase by the same amount. Red color shows PDOS of  $\text{Cu}_2\text{O}$  only, green color shows  $\text{CuAlO}_2$  only, orange color shows both  $\text{Cu}_2\text{O}$  and  $\text{CuAlO}_2$ , and yellow color shows the donor.

between the elemental characterization and XRD patterns. If hexagonal P63mmc is used to describe the structural properties of the  $\text{CuAlO}_2$  sample T200, then the concentration of copper and aluminum must be equal. But this is not the case as shown in Table S3. Since no XRD peak for various copper oxides can be matched with the obtained XRD pattern (shown on Fig. S2), we suggest that the excess of copper oxide would be in an amorphous form. As a consequence, no crystalline peak was observed for all samples exhibiting an excess of copper oxide.

Fig. 3 shows optical characterizations of all  $\text{CuAl}_x\text{O}_y$  films. Firstly, in order to estimate the bandgap of these films, the functions  $(\alpha h\nu)^{1/2}$  are traced against photon energy. The absorption coefficient  $\alpha$  was calculated based on the thicknesses, shown in Table S3, and the absorption spectra. The power 1/2 of  $(\alpha h\nu)$  was chosen for characterizing an indirect bandgap material since we have revealed the amorphous nature of these films combined with a portion of the hexagonal phase of delafossite  $\text{CuAlO}_2$  [38]. Secondly, the Tauc bandgap extrapolation was performed as the crossing point of the linear fit of  $(\alpha h\nu)^{1/2}$  function with the horizontal axis (Fig. 3 from a to c). The values of indirect bandgap of  $\text{CuAl}_x\text{O}_y$  are shown in Table S4. Fig. 3d–f exhibit the comparison of  $I_s$  and  $I_c$  normalized intensities between the experimental spectra and the one obtained by SE adjustment. The dispersion function used to describe  $\text{CuAl}_x\text{O}_y$  is the double amorphous function (the detailed formula are presented in the electronic supplementary information). Values of the double amorphous function parameters ( $\epsilon_\infty$ ,  $E_g$ ,  $A1$ ,  $B1$ ,  $C1$ ,  $A2$ ,  $B2$ ,  $C2$ ) are presented in Table S4 as well as the adjustment quality  $X$  (the smaller the value of  $X$ , the better the adjustment). The parameter  $\epsilon_\infty$  gives an estimation of the real part of the dielectric constant at an infinite photon wavelength. The parameter  $E_g$  is the estimation of the bandgap based on the double amorphous function. There is a good agreement between the experimental intensities ( $I_s$  and  $I_c$ ) with the SE adjustment combined with a relatively low value of  $X$  (in Table S4). The difference in values of bandgap deduced from the extrapolation (Fig. 3a–c) and by the SE adjustment is relatively low. It is worth noting that the thicknesses

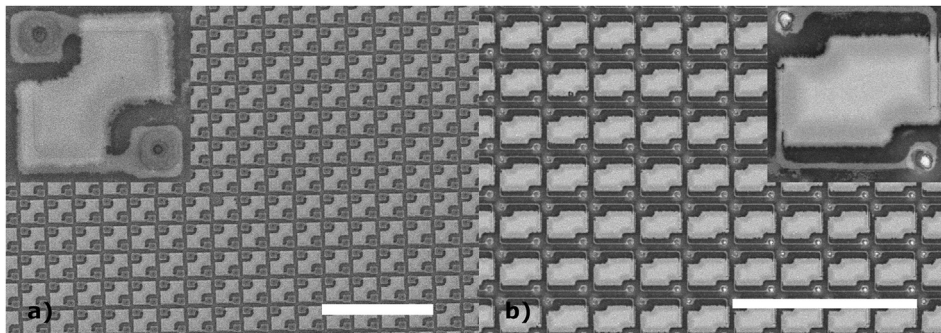
of all samples are taken from the profilometer measurement and used as the fixed input thickness for the SE adjustment. Therefore, the SE adjustment performed here is reliable. Since the application of micro-bolometer is in the long wavelength region (up to 10  $\mu\text{m}$ ), an extrapolation of the refractive indices of all the films was performed as shown in Fig. 3g–i. A good tendency of refractive index when increasing wavelength is obtained for all samples investigated (except for T700). In order to estimate the refractive index of the  $\text{CuAl}_x\text{O}_y$  films in the long wavelength region, we have taken the square root of the average real value of the dielectric constant at the infinite wavelength  $\epsilon_\infty$  for all the samples. This value is equal to  $2.27 \pm 0.07$ , corresponding to  $\epsilon_\infty = 5.15 \pm 0.67$ . The extinction coefficient, on the other hand, is equal to zero for all photon energies smaller than the bandgap value. Thus, we used the zero value in the long wavelength region. The value of the refractive index of  $\text{CuAl}_x\text{O}_y$  deduced here will play a central role in designing the antireflection coating layer on top of the  $\text{CuAl}_x\text{O}_y$  layer when it is used in a real micro-bolometer.

In order to elucidate the low  $\sim 1$  eV indirect band gap of this  $\text{CuAl}_x\text{O}_y$  material, a direct band gap extrapolation was performed with the curves  $(\alpha h\nu)^2$  versus photon energy. Bandgap values of  $\sim 2.8$  eV were obtained, which are comparable with those reported previously for  $\text{CuAlO}_2$  [26]. By combining the n-type nature, direct transitions around 2.8 eV, indirect transitions around 1 eV, and the electronic affinities of  $\text{CuAlO}_2$  (2.5 eV) and  $\text{Cu}_2\text{O}$  (3.2 eV) found in the literature [39,40], a schematic of electronic levels of  $\text{CuAl}_x\text{O}_y$  is illustrated in Fig. 4. The highest levels are the conduction band (CB) of  $\text{CuAlO}_2$ . From the obtained values of activation energy, we can identify a donor band, mainly due to the intentionally sputtered excess of metals in the material, lining from 132 meV to 175 meV below the CB of  $\text{CuAlO}_2$ . The Fermi level needs to be between donor levels and CB, thus all bands below the Fermi level are populated including the Cu-4s and the lower Cu-3d levels of CB of  $\text{Cu}_2\text{O}$  and the valence band of  $\text{Cu}_2\text{O}$  and  $\text{CuAlO}_2$  (based on the reports about the partial density of states (PDOS) of  $\text{Cu}_2\text{O}$  and  $\text{CuAlO}_2$  [41–44]). We suggest that the  $\sim 0.9$ – $1$  eV transition is (i) an intraband and indirect transition in the conduction band of  $\text{Cu}_2\text{O}$  or (ii) a cross transition from the bottom CB of  $\text{Cu}_2\text{O}$  to the CB of  $\text{CuAlO}_2$ . As a result, we propose that this  $\text{CuAl}_x\text{O}_y$  material can be considered as a bulk heterojunction, with type I band alignment, between  $\text{CuAlO}_2$  and  $\text{Cu}_2\text{O}$  in an amorphous matrix. Interestingly, if one could tune the donor levels, for example, to be closer to the bottom of the CB of  $\text{Cu}_2\text{O}$ , one could both increase the conductivity (by more electrons in the CB of  $\text{Cu}_2\text{O}$  embedded in the matrix) and the TCR (by enlarging the activation energy with respect to the CB of  $\text{CuAlO}_2$ ). Finally, we would like to note that all samples became more transparent and much less conductive after annealing under ambient oxygen, thus highlighting the choice of  $\text{Cu}_2\text{O}$  over other types of copper oxides with higher values of oxidation.

Table 1 shows a comparative illustration of several main materials used in functional UFPAs with the  $\text{CuAl}_x\text{O}_y$  material in this paper.  $\text{CuAl}_x\text{O}_y$  thin films have a smaller refractive index in comparison to the refractive index of vanadium oxides in the range from 2.5 to 3 [45,46] and that of amorphous silicon (or polycrystalline germanium silicon) in the range from 3.4 to 3.5 [47], thus they have certain advantage for antireflection in the long

**Table 1**  
Comparative illustration of several main materials in UFPAs.

Material	TCR (%/°C)	Resistivity ( $\Omega\cdot\text{cm}$ )	Refractive index in the LWIR region
VOx	1–3 [37]	0.01–1.0 [37]	2.5–3 [45,46]
a-Si	2–5 [9]	100–10 k [9]	3.4–3.5 [47]
pm-Si <sub>x</sub> Ge <sub>1-x</sub>	4.08 [48]	67 k [48]	N/A (from silicon to germanium) 3.4–4
$\text{CuAl}_x\text{O}_y$ (this work)	1.7–2.2	0.3–1.0	$2.27 \pm 0.07$



**Fig. 5.** SEM micrographs of micro-bolometers with 25  $\mu\text{m}$  pitch obtained by eight photolithography steps with an active layer of  $\text{CuAl}_x\text{O}_y$  and with two different active layer geometries. Inserted images are the corresponding pixels with dimensions of 25  $\mu\text{m} \times 25 \mu\text{m}$ . The scale bars are 100  $\mu\text{m}$ .

wavelength region. In combination with the resistance properties, the  $\text{CuAl}_x\text{O}_y$  films exhibit a slight edge in optical performance versus vanadium oxides and better resistance and optical properties versus amorphous silicon. Furthermore, with an interesting finding discussed earlier in this paper,  $\text{CuAl}_x\text{O}_y$  could be considered as a bulk heterojunction with type I band alignment between  $\text{CuAlO}_2$  and  $\text{Cu}_2\text{O}$  with the ability to increase both the conductivity and TCR at the same time. As a consequence, these  $\text{CuAl}_x\text{O}_y$  films are a strong candidate for use in thermal infrared imagers.

Fig. 5 shows SEM micrographs of arrays of 25- $\mu\text{m}$  micro-bolometers with two different geometries with the  $\text{CuAl}_x\text{O}_y$  film as the active temperature sensing layer. This active layer is sandwiched between a supporting layer and an antireflection encapsulation layer. The supporting layer also includes a layer serving to absorb radiation in the long wavelength region. These arrays were obtained by at least eight photolithography steps for assuring the pattern of (i) row electrical channels, (ii) column electrical channels, (iii) various pathways from the active layer to electrical channels, and (iv) suspending structures for thermal isolation of the active layer in an improved process flow in comparison to our previous study [49]. It can be observed that the good micro-bolometer shapes were obtained, thus assuring that the  $\text{CuAl}_x\text{O}_y$  films are well suited for micro-machining process flow for the fabrication of an array of micro-bolometers. The active layer,  $\text{CuAl}_x\text{O}_y$ , was effectively patterned in the last photolithography step, which assures the maximum stability of the TCR values of  $\text{CuAl}_x\text{O}_y$ . Further studies need to be completed in order to yield (i) a higher TCR value around from 4 to 5%/K, (ii) ohmic contacts between  $\text{CuAl}_x\text{O}_y$  thin films and metal connections, (iii) better etching of  $\text{CuAl}_x\text{O}_y$  thin films, and finally (iv) better releasing of  $\text{CuAl}_x\text{O}_y$  micro-bridges.

#### 4. Conclusion

Our experimental study on the  $\text{CuAl}_x\text{O}_y$  semiconductor has revealed its enormous potential for applications as micro-bolometers and thermal infrared imagers. We found that the reactive sputtering conditions, including substrate temperature and sputtering power, had the remarkable influence on the resistance and optical properties of the  $\text{CuAl}_x\text{O}_y$  films. The value of TCR was found to be around 2%/°C combined with a range of sheet resistance from 12.5  $\text{k}\Omega/\text{square}$  to about 47.5  $\text{k}\Omega/\text{square}$ . The  $\text{CuAl}_x\text{O}_y$  material was of n-type with an activation energy ranging from 132 to 175 meV. The average value of the indirect bandgap was determined to be around 1 eV, which was also confirmed by spectroscopic ellipsometry adjustments. A type-I band alignment bulk heterojunction between  $\text{CuAlO}_2$  and  $\text{Cu}_2\text{O}$  was proposed for explaining this low indirect band gap value. Based on the double

amorphous dispersion function, we obtained an average refractive index value of  $2.27 \pm 0.07$  in the long wavelength region. Regarding the compatibility of  $\text{CuAl}_x\text{O}_y$  with photolithography-based surface micromachining, two different micro-bolometer geometries were fabricated with  $\text{CuAl}_x\text{O}_y$  acting as the active layer. The good micro-bolometer shapes were achieved, enabling the future development of high-performance thermal infrared imaging sensors based on this class of  $\text{CuAl}_x\text{O}_y$  materials.

#### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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#### Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.jsamd.2021.01.004>.

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